DATA SHEET

Datasheet.Company

NE5517/NE5517A

Dual operational transconductance amplifier

Product data
Supersedes data of 1994 Aug 31
File under Integrated Circuits, IC11 Data Handbook





Dual operational transconductance amplifier

NE5517/NE5517A

DESCRIPTION

The NE5517 contains two current-controlled transconductance amplifiers, each with a differential input and push-pull output. The NE5517 offers significant design and performance advantages over similar devices for all types of programmable gain applications. Circuit performance is enhanced through the use of linearizing diodes at the inputs which enable a 10 dB signal-to-noise improvement referenced to 0.5% THD. The NE5517 is suited for a wide variety of industrial and consumer applications and is recommended as the preferred circuit in the Dolby™ HX (Headroom Extension) system.

Constant impedance buffers on the chip allow general use of the NE5517. These buffers are made of Darlington transistor and a biasing network which changes bias current in dependence of I_{ABC} .

Therefore, changes of output offset voltages are almost eliminated. This is an advantage of the NE5517 compared to LM13600. With the LM13600, a burst in the bias current I_{ABC} guides to an audible offset voltage change at the output. With the constant impedance buffers of the NE5517 this effect can be avoided and makes this circuit preferable for high quality audio applications.

FEATURES

- Constant impedance buffers
- \bullet ΔV_{BE} of buffer is constant with amplifier I_{BIAS} change
- Pin compatible with LM13600
- Excellent matching between amplifiers
- Linearizing diodes
- High output signal-to-noise ratio

APPLICATIONS

- Multiplexers
- Timers
- Electronic music synthesizers
- Dolby™ HX Systems
- Current-controlled amplifiers, filters
- Current-controlled oscillators, impedances

PIN CONFIGURATION

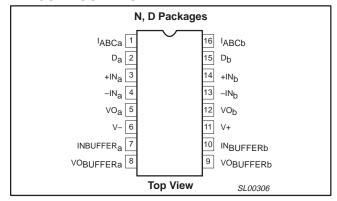


Figure 1. Pin Configuration

PIN DESIGNATION

PIN NO.	SYMBOL	NAME AND FUNCTION
1	I _{ABCa}	Amplifier bias input A
2	Da	Diode bias A
3	+IN _a	Non-inverting input A
4	-IN _a	Inverting input A
5	V _{Oa}	Output A
6	V-	Negative supply
7	IN _{BUFFERa}	Buffer input A
8	VO _{BUFFERa}	Buffer output A
9	VO _{BUFFERb}	Buffer output B
10	IN _{BUFFERb}	Buffer input B
11	V+	Positive supply
12	V _{Ob}	Output B
13	-IN _b	Inverting input B
14	+IN _b	Non-inverting input B
15	D _b	Diode bias B
16	I _{ABCb}	Amplifier bias input B

ORDERING INFORMATION

DESCRIPTION	TEMPERATURE RANGE	ORDER CODE	DWG #
16-Pin Plastic Dual In-Line Package (DIP)	0 to +70 °C	NE5517N	SOT38-4
16-Pin Plastic Dual In-Line Package (DIP)	0 to +70 °C	NE5517AN	SOT38-4
16-Pin Small Outline (SO) Package	0 to +70 °C	NE5517D	SOT109-1

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CIRCUIT SCHEMATIC

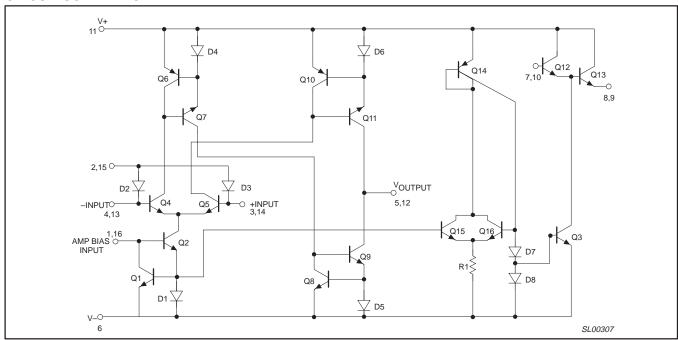


Figure 2. Circuit Schematic

CONNECTION DIAGRAM

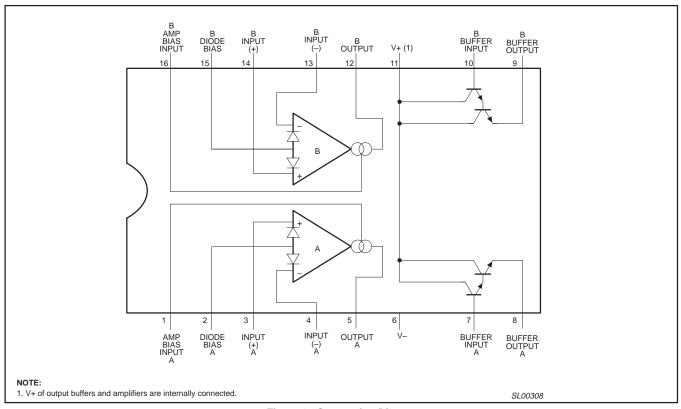


Figure 3. Connection Diagram

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ABSOLUTE MAXIMUM RATINGS

SYMBOL	PARAMETER	RATING	UNIT
V _S	Supply voltage ¹ NE5517 NE5517A	36 V _{DC} or ±18 44 V _{DC} or ±22	V V
P _D	Power dissipation, $T_{amb} = 25 ^{\circ}\text{C (still air)}^2$ NE5517N, NE5517AN NE5517D	1500 1125	mW mW
V _{IN}	Differential input voltage	±5	V
I _D	Diode bias current	2	mA
I _{ABC}	Amplifier bias current	2	mA
I _{SC}	Output short-circuit duration	Indefinite	
I _{OUT}	Buffer output current ³	20	mA
T _{amb}	Operating temperature range NE5517N, NE5517AN	0 °C to +70 °C	°C
V_{DC}	DC input voltage	+V _S to -V _S	
T _{stg}	Storage temperature range	−65 °C to +150 °C	°C
T _{sld}	Lead soldering temperature (10 sec max)	230	°C

NOTES:

^{1.} For selections to a supply voltage above ±22 V, contact factory
2. The following derating factors should be applied above 25 °C

N package at 12.0 mW/°C

D package at 9.0 mW/°C

3. Buffer output current should be limited so as to not exceed package dissipation.

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DC ELECTRICAL CHARACTERISTICS1

OVMDOL	DADAMETED	TEST SOMBITIONS		NE5517			NE5517A	1	LINIT
SYMBOL	PARAMETER	TEST CONDITIONS	Min	Тур	Max	Min	Тур	Max	UNIT
				0.4	5		0.4	2	mV
Vos	Input offset voltage	Over temperature range			_			5	mV
		I _{ABC} 5 μA		0.3	5		0.3	2	mV
	ΔV _{OS} /ΔT	Avg. TC of input offset voltage		7			7		μV/°C
	V _{OS} including diodes	Diode bias current (I_D) = 500 μ A		0.5	5		0.5	2	mV
Vos	Input offset change	5 μA ≤ I _{ABC} ≤ 500 μA		0.1			0.1	3	mV
los	Input offset current			0.1	0.6		0.1	0.6	μΑ
	ΔI _{OS} /ΔT	Avg. TC of input offset current		0.001			0.001		μΑ/°C
I _{BIAS}	Input bias current	Over temperature range		0.4 1	5 8		0.4 1	5 7	μA μA
	$\Delta I_{B}/\Delta T$	Avg. TC of input current		0.01			0.01		μΑ/°C
9м	Forward transconductance	Over temperature range	6700 5400	9600	1300	7700 4000	9600	1200	μmho μmho
	g _M tracking			0.3			0.3		dB
I _{OUT}	Peak output current	$R_L = 0$, $I_{ABC} = 5 \mu A$ $R_L = 0$, $I_{ABC} = 500 \mu A$ $R_L = 0$	350 300	5 500	650	3 350 300	5 500	7 650	μΑ μΑ μΑ
V _{OUT}	Peak output voltage Positive Negative	$R_L = \infty$, 5 μA ≤ $I_{ABC} \le 500$ μA $R_L = \infty$, 5 μA ≤ $I_{ABC} \le 500$ μA	+12 -12	+14.2 -14.4		+12 -12	+14.2 -14.4		V V
I _{CC}	Supply current	I _{ABC} = 500 μA, both channels		2.6	4		2.6	4	mA
	V _{OS} sensitivity Positive Negative	Δ V _{OS} /Δ V+ Δ V _{OS} /Δ V-		20 20	150 150		20 20	150 150	μV/V μV/V
CMRR	Common-mode rejection ration		80	110		80	110		dB
	Common-mode range		±12	±13.5		±12	±13.5		V
	Crosstalk	Referred to input ² 20 Hz < f < 20 kHz		100			100		dB
I _{IN}	Differential input current	$I_{ABC} = 0$, input = $\pm 4 \text{ V}$		0.02	100		0.02	10	nA
	Leakage current	I _{ABC} = 0 (Refer to test circuit)		0.2	100		0.2	5	nA
R _{IN}	Input resistance	,	10	26		10	26		kΩ
B _W	Open-loop bandwidth			2			2		MHz
SR	Slew rate	Unity gain compensated		50			50		V/μs
IN _{BUFFER}	Buffer input current	5		0.4	5		0.4	5	μА
VO _{BUFFER}	Peak buffer output voltage	5	10	 		10	<u> </u>		V
- DOLLEIV	ΔV _{BE} of buffer	Refer to Buffer V _{BE} test circuit ³	<u> </u>	0.5	5	<u> </u>	0.5	5	mV

NOTES:

These specifications apply for V_S = ±15 V, T_{amb} = 25 °C, amplifier bias current (I_{ABC}) = 500 μA, Pins 2 and 15 open unless otherwise specified. The inputs to the buffers are grounded and outputs are open.
 These specifications apply for V_S = ±15 V, I_{ABC} = 500 μA, R_{OUT} = 5 kΩ connected from the buffer output to -V_S and the input of the buffer is connected to the transconductance amplifier output.
 V_S = ±15, R_{OUT} = 5 kΩ connected from Buffer output to -V_S and 5 μA ≤ I_{ABC} ≤ 500 μA.

TYPICAL PERFORMANCE CHARACTERISTICS

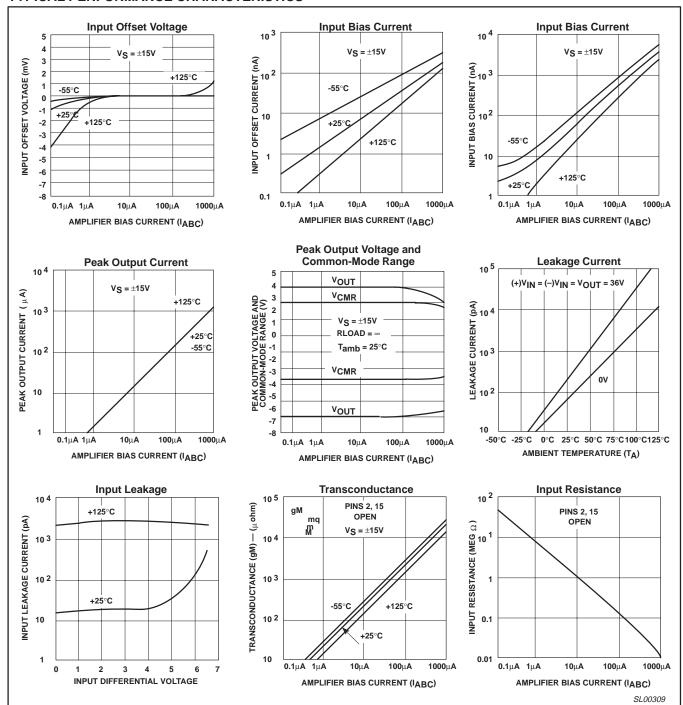


Figure 4. Typical Performance Characteristics

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TYPICAL PERFORMANCE CHARACTERISTICS (Continued)

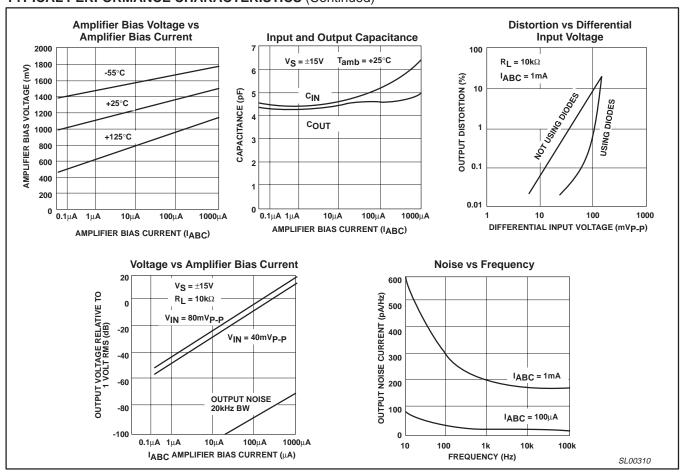


Figure 5. Typical Performance Characteristics (cont.)

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TYPICAL PERFORMANCE CHARACTERISTICS (Continued)

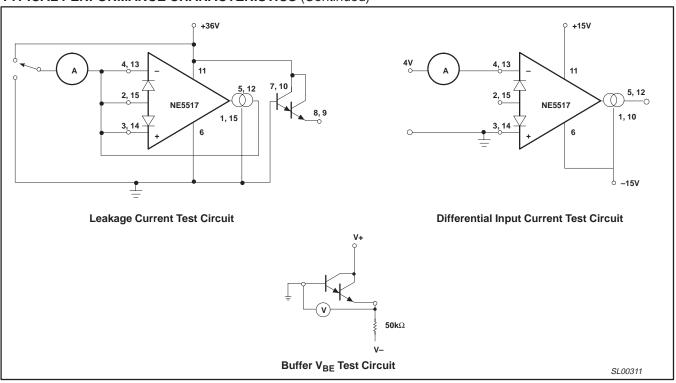


Figure 6. Typical Performance Characteristics (cont.)

APPLICATIONS

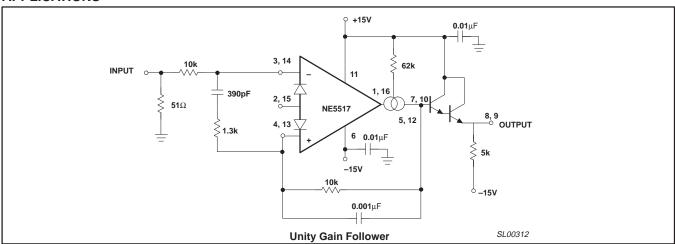


Figure 7. Applications

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CIRCUIT DESCRIPTION

The circuit schematic diagram of one-half of the NE5517, a dual operational transconductance amplifier with linearizing diodes and impedance buffers, is shown in Figure 8.

1. Transconductance Amplifier

The transistor pair, Q_4 and Q_5 , forms a transconductance stage. The ratio of their collector currents (I_4 and I_5 , respectively) is defined by the differential input voltage, V_{IN} , which is shown in equation 1.

$$V_{IN} = \frac{KT}{q} \ln \frac{I_5}{I_4}$$
 (1)

Where V_{IN} is the difference of the two input voltages

KT ≈ 26 mV at room temperature (300 °k).

Transistors Q_1 , Q_2 and diode D_1 form a current mirror which focuses the sum of current I_4 and I_5 to be equal to amplifier bias current I_B :

$$I_4 + I_5 = I_B$$
 (2)

If V_{IN} is small, the ratio of I_5 and I_4 will approach unity and the Taylor series of In function can be approximated as

$$\frac{\mathsf{KT}}{\mathsf{q}} \ln \frac{\mathsf{I}_5}{\mathsf{I}_4} \approx \frac{\mathsf{KT}}{\mathsf{q}} \frac{\mathsf{I}_5 - \mathsf{I}_4}{\mathsf{I}_4} \tag{3}$$

and $I_4 \cong I_5 \cong I_B$

$$\begin{split} \frac{KT}{q} & \ln \frac{I_5}{I_4} \approx \frac{KT}{q} \frac{I_5 - I_4}{1/2I_B} = \frac{2KT}{q} \frac{I_5 - I_4}{I_B} = V_{IN}^{(4)} \\ & I_5 - I_4 = V_{IN} \frac{\left(I_B^q\right)}{2KT} \end{split}$$

The remaining transistors (Q_6 to Q_{11}) and diodes (D_4 to D_6) form three current mirrors that produce an output current equal to I_5 minus I_4 . Thus:

$$V_{IN}\left(I_{B}\frac{q}{2KT}\right) = I_{O} \tag{5}$$

The term $\frac{\left(I_B^{\ q}\right)}{2KT}$ is then the transconductance of the amplifier and is proportional to I_B .

2. Linearizing Diodes

For V_{IN} greater than a few millivolts, equation 3 becomes invalid and the transconductance increases non-linearly. Figure 9 shows how the internal diodes can linearize the transfer function of the operational amplifier. Assume D_2 and D_3 are biased with current sources and the input signal current is I_{S} . Since

 $I_4 + I_5 = I_B$ and $I_5 - I_4 = I_0$, that is:

$$I_4 = (I_B - I_0), I_5 = (I_B + I_0)$$

For the diodes and the input transistors that have identical geometries and are subject to similar voltages and temperatures, the following equation is true:

$$\frac{T}{q} \ln \frac{\frac{I_D}{2} + I_S}{\frac{I_D}{2} - I_S} = \frac{KT}{q} \ln \frac{1/2(I_B + I_O)}{1/2(I_B - I_O)}$$
(6)

$$I_{O} = I_{S} \frac{2^{I}B}{I_{D}} \text{ for } |I_{S}| < \frac{I_{D}}{2}$$

The only limitation is that the signal current should not exceed I_D.

3. Impedance Buffer

The upper limit of transconductance is defined by the maximum value of I_B (2 mA). The lowest value of I_B for which the amplifier will function therefore determines the overall dynamic range. At low values of I_B , a buffer with very low input bias current is desired. A Darlington amplifier with constant-current source ($Q_{14}, Q_{15}, Q_{16}, D_7, D_8$, and R_1) suits the need.

APPLICATIONS

Voltage-Controlled Amplifier

In Figure 10, the voltage divider R_2 , R_3 divides the input-voltage into small values (mV range) so the amplifier operates in a linear manner.

It is:

$$I_{OUT} = -V_{IN} \cdot \frac{R_3}{R_2 + R_3} \cdot gM;$$

$$V_{OUT} = I_{OUT} \cdot R_{L};$$

$$A = \frac{V_{OUT}}{V_{IN}} = \frac{R_3}{R_2 + R_3} \cdot gM \cdot R_L$$

(3)
$$g_M = 19.2 I_{ABC}$$

(g_M in μ mhos for I_{ABC} in mA)

Since g_M is directly proportional to I_{ABC} , the amplification is controlled by the voltage V_C in a simple way.

When V_C is taken relative to -V_{CC} the following formula is valid:

$$I_{ABC} = \frac{(V_C - 1.2V)}{R_1}$$

The 1.2 V is the voltage across two base-emitter baths in the current mirrors. This circuit is the base for many applications of the NE5517.

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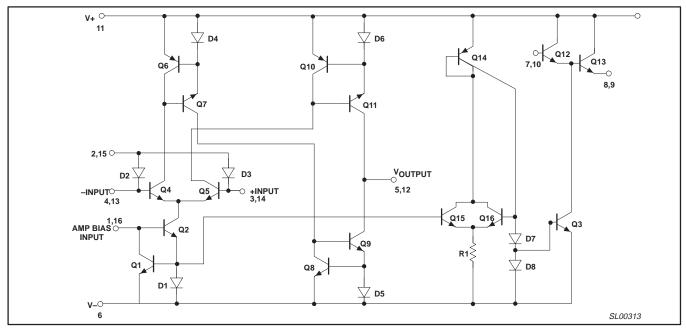


Figure 8. Circuit Diagram of NE5517

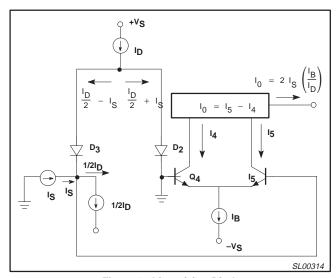


Figure 9. Linearizing Diode

Stereo Amplifier With Gain Control

Figure 11 shows a stereo amplifier with variable gain via a control input. Excellent tracking of typical 0.3 dB is easy to achieve. With the potentiometer, $R_{P_{1}}$ the offset can be adjusted. For AC-coupled amplifiers, the potentiometer may be replaced with two 510 Ω resistors.

Modulators

Because the transconductance of an OTA (Operational Transconductance Amplifier) is directly proportional to I_{ABC} , the amplification of a signal can be controlled easily. The output current is the product from transconductance×input voltage. The circuit is effective up to approximately 200 kHz. Modulation of 99% is easy to achieve.

Voltage-Controlled Resistor (VCR)

Because an OTA is capable of producing an output current proportional to the input voltage, a voltage variable resistor can be made. Figure 13 shows how this is done. A voltage presented at the R_X terminals forces a voltage at the input. This voltage is multiplied by g_M and thereby forces a current through the R_X terminals:

$$R_{X} = \frac{R + R_{A}}{gM + R_{\Delta}}$$

where g_M is approximately 19.21 μ MHOs at room temperature. Figure 14 shows a Voltage Controlled Resistor using linearizing diodes. This improves the noise performance of the resistor.

Voltage-Controlled Filters

Figure 15 shows a Voltage Controlled Low-Pass Filter. The circuit is a unity gain buffer until X_C/g_M is equal to R/R_A . Then, the frequency response rolls off at a 6dB per octave with the -3 dB point being defined by the given equations. Operating in the same manner, a Voltage Controlled High-Pass Filter is shown in Figure 16. Higher order filters can be made using additional amplifiers as shown in Figures 17 and 18.

Voltage-Controlled Oscillators

Figure 19 shows a voltage-controlled triangle-square wave generator. With the indicated values a range from 2 Hz to 200 kHz is possible by varying $I_{\mbox{\footnotesize{ABC}}}$ from 1 mA to 10 $\mu\mbox{\footnotesize{A}}.$

The output amplitude is determined by $I_{\text{OUT}} \times R_{\text{OUT}}$.

Please notice the differential input voltage is not allowed to be above 5 $\rm V.$

With a slight modification of this circuit you can get the sawtooth pulse generator, as shown in Figure 20.

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APPLICATION HINTS

To hold the transconductance g_M within the linear range, I_{ABC} should be chosen not greater than 1 mA. The current mirror ratio should be as accurate as possible over the entire current range. A current mirror with only two transistors is not recommended. A suitable current mirror can be built with a PNP transistor array which causes excellent matching and thermal coupling among the

transistors. The output current range of the DAC normally reaches from 0 to -2 mA. In this application, however, the current range is set through R_{REF} (10 $k\Omega)$ to 0 to -1 mA.

$$I_{DACMAX} = 2 \cdot \frac{V_{REF}}{R_{REF}} = 2 \cdot \frac{5V}{10k\Omega} = 1mA$$

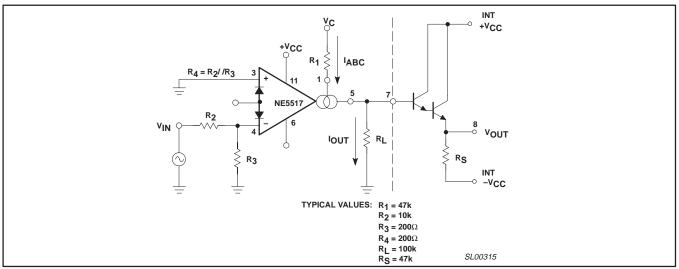


Figure 10.

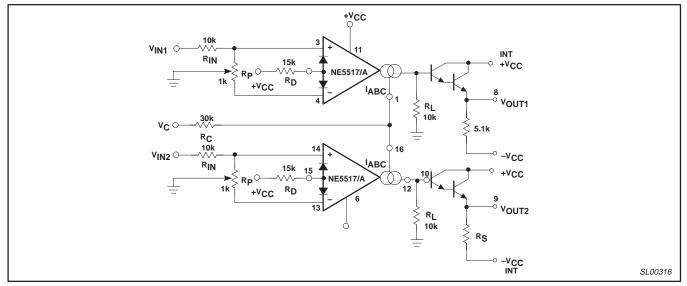


Figure 11. Gain-Controlled Stereo Amplifier

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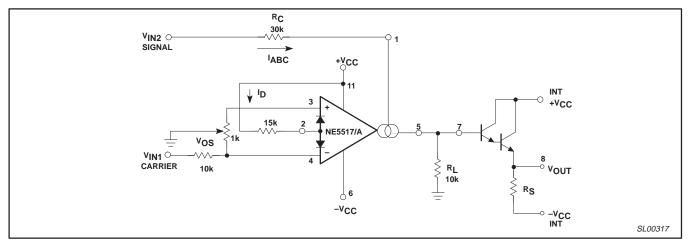


Figure 12. Amplitude Modulator

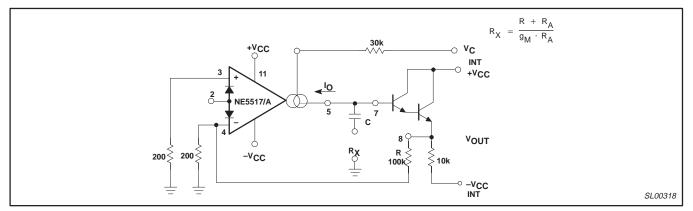


Figure 13. VCR

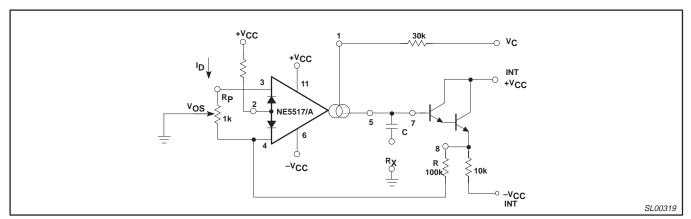


Figure 14. VCR with Linearizing Diodes

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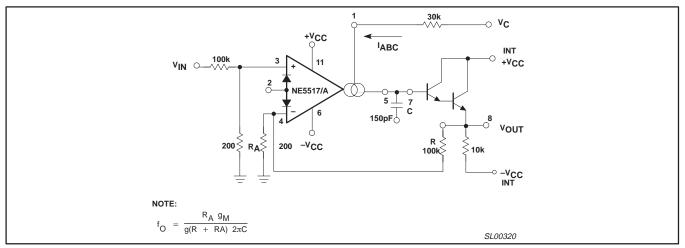


Figure 15. Voltage-Controlled Low-Pass Filter

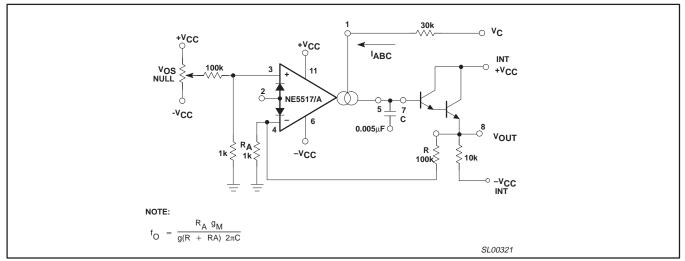


Figure 16. Voltage-Controlled High-Pass Filter

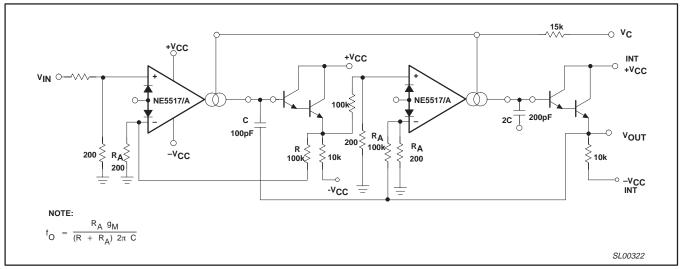


Figure 17. Butterworth Filter - 2nd Order

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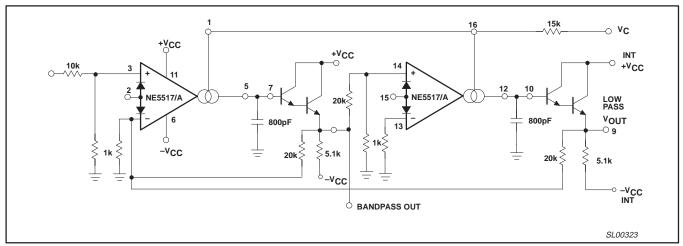


Figure 18. State Variable Filter

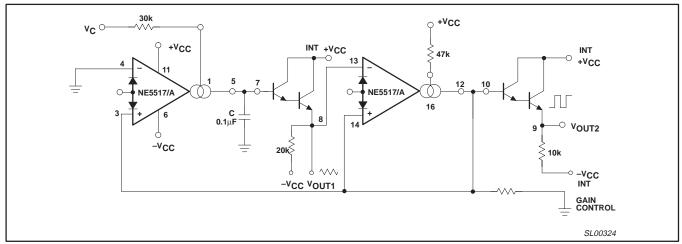


Figure 19. Triangle-Square Wave Generator (VCO)

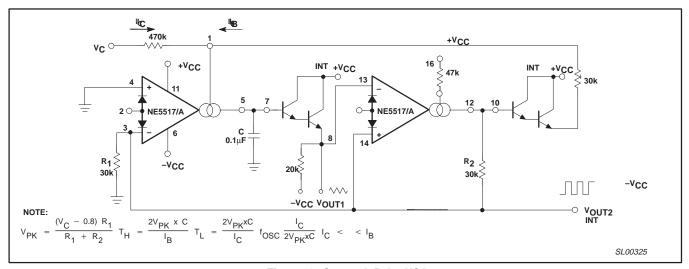


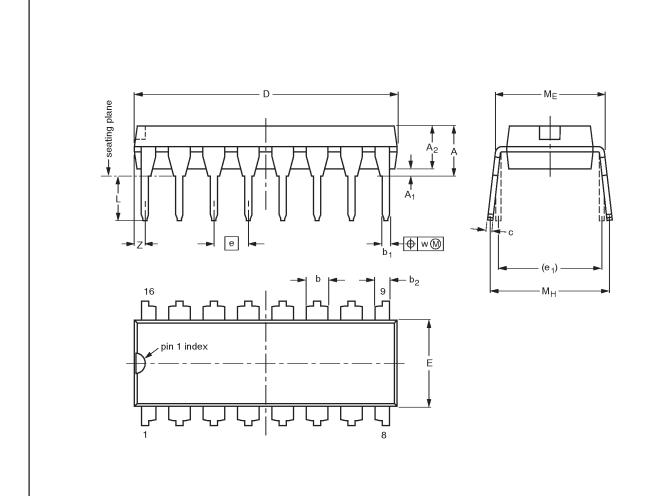
Figure 20. Sawtooth Pulse VCO

Dual operational transconductance amplifier

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DIP16: plastic dual in-line package; 16 leads (300 mil)

SOT38-4



DIMENSIONS (inch dimensions are derived from the original mm dimensions)

UNIT	A max.	A ₁ min.	A ₂ max.	b	b ₁	b ₂	С	D ⁽¹⁾	E ⁽¹⁾	е	e ₁	L	ME	Мн	w	Z ⁽¹⁾ max.
mm	4.2	0.51	3.2	1.73 1.30	0.53 0.38	1.25 0.85	0.36 0.23	19.50 18.55	6.48 6.20	2.54	7.62	3.60 3.05	8.25 7.80	10.0 8.3	0.254	0.76
inches	0.17	0.020	0.13	0.068 0.051	0.021 0.015	0.049 0.033	0.014 0.009	0.77 0.73	0.26 0.24	0.10	0.30	0.14 0.12	0.32 0.31	0.39 0.33	0.01	0.030

10 mm

Note

1. Plastic or metal protrusions of 0.25 mm maximum per side are not included.

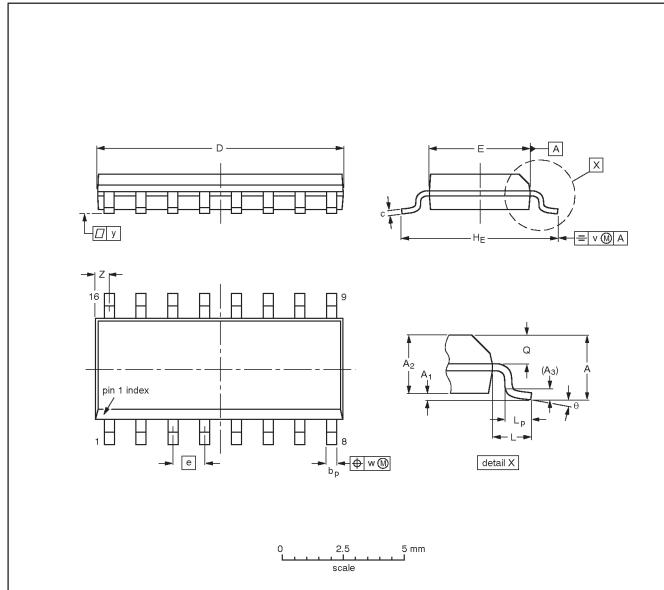
OUTLINE		REFER	EUROPEAN	ISSUE DATE		
VERSION	IEC	JEDEC	EIAJ		PROJECTION	ISSUE DATE
SOT38-4						-92-11-17 95-01-14

Dual operational transconductance amplifier

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SO16: plastic small outline package; 16 leads; body width 3.9 mm

SOT109-1



DIMENSIONS (inch dimensions are derived from the original mm dimensions)

UNIT	A max.	A ₁	A ₂	A ₃	bp	С	D ⁽¹⁾	E ⁽¹⁾	е	HE	L	Lp	Q	٧	w	у	Z ⁽¹⁾	θ
mm	1.75	0.25 0.10	1.45 1.25	0.25	0.49 0.36	0.25 0.19	10.0 9.8	4.0 3.8	1.27	6.2 5.8	1.05	1.0 0.4	0.7 0.6	0.25	0.25	0.1	0.7 0.3	8°
inches	0.069	0.010 0.004	0.057 0.049	0.01		0.0100 0.0075	0.39 0.38	0.16 0.15	0.050	0.244 0.228	0.041	0.039 0.016	0.028 0.020	0.01	0.01	0.004	0.028 0.012	0°

Note

1. Plastic or metal protrusions of 0.15 mm maximum per side are not included.

OUTLINE		REFER	EUROPEAN	ISSUE DATE	
VERSION	IEC	JEDEC	EIAJ	PROJECTION	1330E DATE
SOT109-1	076E07	MS-012			97-05-22 99-12-27

Dual operational transconductance amplifier

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NOTES

Dual operational transconductance amplifier

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Data sheet status

Data sheet status ^[1]	Product status ^[2]	Definitions
Objective data	Development	This data sheet contains data from the objective specification for product development. Philips Semiconductors reserves the right to change the specification in any manner without notice.
Preliminary data	Qualification	This data sheet contains data from the preliminary specification. Supplementary data will be published at a later date. Philips Semiconductors reserves the right to change the specification without notice, in order to improve the design and supply the best possible product.
Product data	Production	This data sheet contains data from the product specification. Philips Semiconductors reserves the right to make changes at any time in order to improve the design, manufacturing and supply. Changes will be communicated according to the Customer Product/Process Change Notification (CPCN) procedure SNW-SQ-650A.

^[1] Please consult the most recently issued data sheet before initiating or completing a design.

Definitions

Short-form specification — The data in a short-form specification is extracted from a full data sheet with the same type number and title. For detailed information see the relevant data sheet or data handbook.

Limiting values definition — Limiting values given are in accordance with the Absolute Maximum Rating System (IEC 60134). Stress above one or more of the limiting values may cause permanent damage to the device. These are stress ratings only and operation of the device at these or at any other conditions above those given in the Characteristics sections of the specification is not implied. Exposure to limiting values for extended periods may affect device reliability.

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^[2] The product status of the device(s) described in this data sheet may have changed since this data sheet was published. The latest information is available on the Internet at URL http://www.semiconductors.philips.com.